







- > Objective : measuring the "true" input impedance
- Setup and VNA calibration process
- Correction calculation
- Results
- Published Papers



## **Objective : measuring the "true" input impedance**

- LISN : Measurement of input impedance Z LISN
  - > The input impedance has to be measured at EUT port:





LISN: single phase





Import data into Excel file



$$\Gamma_{\text{LISN}} = \frac{S_{11} - \Gamma_{in}}{S_{22}(S_{11} - \Gamma_{in}) - S_{12}S_{21}}$$

Correction calculation performed using a specific Excel file



\* (0)

- at	A	В	С	D	E	F	G	H	I	J	K	L
1		MEASUR	REMENT 1	MEASUR	EMENT 2	MEASUF	REMENT 3	MEASUR	EMENT 4	MEASUR	EMENT 5	
2	FREQUENCY (Hz)	Re (Γ)	lm (Γ)	Re (Γ)	lm (Γ)	Re (Γ)	lm (Γ)	Re (Γ)	lm (Γ)	Re (Γ)	lm (Γ)	
3	9000	-0.80061	0.079804	-0.80089	0.079277	-0.80066	0.07912	-0.80038	0.07916	-0.80078	0.079516	
4	9107	-0.80026	0.079756	-0.8	0.079631	-0.7999	0.080094	-0.8001	0.080003	-0.8002	0.080163	
5	9214	-0.80091	0.079926	-0.80036	0.0802	-0.8008	0.079526	-0.80068	0.079762	-0.8007	0.079893	
6	9322	-0.80116	0.080624	-0.80061	0.080278	-0.80071	0.080741	-0.8012	0.080735	-0.80148	0.080743	
7	9429	-0.8014	0.081036	-0.80059	0.081096	-0.80108	0.08084	-0.80137	0.0809	-0.80113	0.080979	
8	9536	-0.8017	0.081119	-0.80151	0.081179	-0.8014	0.081717	-0.80149	0.081381	-0.80178	0.081397	
9	9643	-0.80171	0.081355	- <mark>0.8016</mark> 3	0.081372	-0.80136	0.081424	-0.80192	0.081249	-0.80165	0.081368	
10	9751	-0.80199	0.082095	-0.80161	0.081777	-0.80213	0.081946	-0.80164	0.081789	-0.80201	0.081883	
11	9858	-0.80206	0.082366	-0.80127	0.082458	-0.80144	0.082172	-0.80139	0.082657	-0.80121	0.081876	
12	9965	-0.80177	0.082667	-0.80153	0.082844	-0.80134	0.082431	-0.80156	0.082353	-0.80203	0.083133	
13	10072	-0.80177	0.083036	-0.80169	0.082621	-0.80182	0.083141	-0.80166	0.08296	-0.80202	0.082668	
14	10180	-0.80191	0.083864	-0.8016	0.083579	-0.80191	0.083972	-0.80191	0.08348	-0.80169	0.083664	
15	10287	-0.80245	0.084301	- <mark>0.8024</mark> 9	0.084075	-0.80212	0.084442	-0.80271	0.08424	-0.80247	0.084279	
16	10394	-0.80262	0.084561	-0.80191	0.084422	-0.80243	0.084373	-0.80226	0.084449	-0.8025	0.08446	
17	10501	-0.80277	0.085016	-0.80212	0.085255	-0.80237	0.085281	-0.80285	0.085404	-0.80192	0.085222	
18	10608	-0.80244	0.085986	- <mark>0.8</mark> 0211	0.085812	-0.80191	0.085778	-0.80254	0.085822	- <mark>0.8</mark> 0252	0.085693	
19	10716	-0.80232	0.085878	-0.80204	0.086026	-0.8015	0.086092	-0.80242	0.086395	-0.80214	0.086104	
20	10823	-0.80258	0.087108	-0.80285	0.087217	-0.80213	0.087188	-0.80286	0.087033	-0.80278	0.087153	
21	10930	-0.80289	0.087387	-0.80238	0.087726	-0.80255	0.087517	-0.80289	0.087594	-0.80274	0.087842	
22	11037	-0.80235	0.088417	- <mark>0.8</mark> 0263	0.088894	-0.8025	0.08818	- <mark>0.8</mark> 0259	0.08862	- <mark>0.8</mark> 0259	0.088395	
23	11145	-0.80255	0.088805	-0.80222	0.08842	-0.8024	0.088996	-0.80254	0.088787	-0.80332	0.088586	
24	11252	-0.8034	0.089952	-0.80246	0.089692	-0.80264	0.089748	-0.80296	0.08945	-0.80275	0.089396	
25	11359	-0.80277	0.090142	-0.80228	0.089918	-0.80234	0.089915	-0.80302	0.090014	-0.80262	0.090333	
26	11466	- <mark>0.8035</mark> 3	0.091064	- <mark>0.8</mark> 0286	0.090951	-0.80299	0.091093	- <mark>0.8033</mark> 3	0.091084	-0.8031	0.091293	
27	11573	-0.8027	0.091679	-0.8023	0.091809	-0.80233	0.091874	-0.80313	0.091986	- <mark>0.8023</mark> 9	0.091756	
28	11681	-0.80295	0.091784	-0.80282	0.091931	-0.80245	0.09195	-0.80245	0.09228	-0.80302	0.091987	
29	11788	-0.80255	0.093434	-0.80222	0.093412	-0.80227	0.093812	-0.80249	0.09357	-0.80234	0.093857	
30	11895	-0.8028	0.094101	-0.8026	0.09374	-0.80221	0.09426	-0.80283	0.093977	-0.80313	0.094102	
31	12002	-0.80287	0.094622	-0.80231	0.094382	-0.80236	0.095046	-0.80257	0.094836	-0.80284	0.094729	
32	12110	-0.80272	0.094715	-0.80189	0.094876	-0.80178	0.095094	-0.80232	0.095042	-0.80248	0.095017	
33	12217	-0.80253	0.096558	-0.8024	0.096512	-0.80243	0.096336	-0.80241	0.096243	-0.80214	0.096375	
34	12324	-0.80253	0.096741	- <mark>0.8</mark> 0253	0.096931	-0.80231	0.096923	-0.80232	0.09694	-0.80221	0.096734	
35	12450	-0.80266	0.097843	-0.80254	0.09791	-0.80193	0.097134	-0.80221	0.097978	- <mark>0.8024</mark> 3	0.097739	
36	12598	-0.80207	0.098927	-0.80173	0.098976	-0.80182	0.098966	-0.80156	0.099018	-0.80202	0.098971	
14 4	► N ESH3 RESULT	S SUMMARY	ESH3 RESU	TS SMAT	RIX ESH3	SH3 MEAS	ESH2 RESULT	S SUMMARY	ESH2 RESUL	TS SMAT	RIX ESH2 ES	H2 MEAS



1000

#### > S matrix of each adapter calculated at each frequency

1	S MAT	RIX OF THE AD	APTER CALCU	LATED WITH	THE FREQUENC	CIES OF THE SI	HEET "ESH3 ME	ASUREMENTS'	UNCERTAINTY B OF INPUT IMPEDANCE CALCULATED WITH THE FREQUENCIES OF THE SHEET "ESH3 MEASUREMENTS"						
2	FREQUENCY (Hz)	Re (S <sub>11</sub> )	Im (S <sub>11</sub> )	Re (S <sub>12</sub> )	Im (S <sub>12</sub> )	Re (S <sub>21</sub> )	Im (S <sub>21</sub> )	Re (S <sub>22</sub> )	Im (S <sub>22</sub> )	FREQUENCY (Hz)	UB( Z <sub>IN</sub>  )	$UB(\phi(Z_{IN}))$			
3	9000	-1.2131E-06	1.06869E-05	1	-1.82362E-05	1	-1.82427E-05	-1.62617E-06	1.07095E-05	9000	1.15E-03	4.75E-03			
4	9107	-1.213E-06	1.08164E-05	1	-1.84551E-05	1	-1.84616E-05	-1.62605E-06	1.0839E-05	9107	1.15E-03	4.75E-03			
5	9214	-1.2129E-06	1.09459E-05	1	-1.86741E-05	1	-1.86805E-05	-1.62593E-06	1.09685E-05	9214	1.15E-03	4.75E-03			
6	9322	-1.2128E-06	1.10766E-05	1	-1.8895E-05	1	-1.89015E-05	-1.62581E-06	1.10993E-05	9322	1.15E-03	4.75E-03			
7	9429	-1.2127E-06	1.12061E-05	1	-1.91139E-05	1	-1.91204E-05	-1.62569E-06	1.12288E-05	9429	1.16E-03	4.75E-03			
8	9536	-1.2126E-06	1.13357E-05	1	-1.93328E-05	1	-1.93393E-05	-1.62556E-06	1.13583E-05	9536	1.16E-03	4.75E-03			
9	9643	-1.2125E-06	1.14652E-05	1	-1.95517E-05	1	-1.95582E-05	-1.62544E-06	1.14878E-05	9643	1.16E-03	4.75E-03			
10	9751	-1.2124E-06	1.15959E-05	1	-1.97727E-05	1	-1.97791E-05	-1.62532E-06	1.16185E-05	9751	1.16E-03	4.75E-03			
11	9858	-1.2124E-06	1.17254E-05	1	-1.99916E-05	1	-1.99981E-05	-1.6252E-06	1.1748E-05	9858	1.16E-03	4.75E-03			
12	9965	-1.2123E-06	1.18549E-05	1	-2.02105E-05	1	-2.0217E-05	-1.62508E-06	1.18775E-05	9965	1.16E-03	4.76E-03			
13	10072	-1.2122E-06	1.19844E-05	1	-2.04294E-05	1	-2.04359E-05	-1.62495E-06	1.20071E-05	10072	1.16E-03	4.76E-03			
14	10180	-1.2121E-06	1.21152E-05	1	-2.06504E-05	1	-2.06568E-05	-1.62483E-06	1.21378E-05	10180	1.16E-03	4.76E-03			
15	10287	-1.212E-06	1.22447E-05	1	-2.08693E-05	1	-2.08757E-05	-1.62471E-06	1.22673E-05	10287	1.17E-03	4.76E-03			
16	10394	-1.2119E-06						.62459E-06	1.23968E-05	10394					
17	10501	-1.2118E-06	S matrix		of th	a ad	apter	.62447E-06	1.25263E-05	10501	Type R uncer	rtainty of 7in			
18	10608	-1.2117E-06	Omathy			e au		.62435E-06	1.26558E-05	10608	Type D uncer				
19	10716	-1.2116E-06	1.2/039E-00	1	-2.1/4/E-UD	1	-2.1/334E-U3	-1.62422E-06	1.27866E-05	10716	Magnituda				
20	10823	-1.2115E-06	1.28934E-05 1 - 1.3023E-05 1 -		-2.19659E-05	1	-2.19723E-05	-1.6241E-06	1.29161E-05	10823	Magnitude	and phase			
21	10930	-1.2114E-06			-2.21848E-05	1	-2.21913E-05	-1.62398E-06	1.30456E-05	10930	U I				
22	11037	-1.2113E-06	1.31525E-05	1	-2.24037E-05	1	-2.24102E-05	-1.62386E-06	1.31751E-05	11037	1.17E-03	4.77E-03			
23	11145	-1.2112E-06	1.32832E-05	1	-2.26247E-05	1	-2.26311E-05	-1.62373E-06	1.33058E-05	11145	1.18E-03	4.77E-03			
24	11252	-1.2111E-06	1.34127E-05	1	-2.28436E-05	1.0000001	-2.285E-05	-1.62361E-06	1.34353E-05	11252	1.18E-03	4.77E-03			
25	11359	-1.211E-06	1.35422E-05	1	-2.30625E-05	1.0000001	-2.3069E-05	-1.62349E-06	1.35648E-05	11359	1.18E-03	4.77E-03			
26	11466	-1.2109E-06	1.36717E-05	1	-2.32814E-05	1.0000001	-2.32879E-05	-1.62337E-06	1.36944E-05	11466	1.18E-03	4.77E-03			
27	11573	-1.2108E-06	1.38012E-05	1	-2.35003E-05	1.0000001	-2.35068E-05	-1.62325E-06	1.38239E-05	11573	1.18E-03	4.77E-03			
28	11681	-1.2107E-06	1.3932E-05	1	-2.37213E-05	1.0000001	-2.37277E-05	-1.62312E-06	1.39546E-05	11681	1.18E-03	4.77E-03			
29	11788	-1.2106E-06	1.40615E-05	1	-2.39402E-05	1.0000001	-2.39466E-05	-1.623E-06	1.40841E-05	11788	1.18E-03	4.77E-03			
30	11895	-1.2105E-06	1.4191E-05	1	-2.41591E-05	1.0000001	-2.41656E-05	-1.62288E-06	1.42136E-05	11895	1.18E-03	4.78E-03			
31	12002	-1.2104E-06	1.43205E-05	1	-2.4378E-05	1.0000001	-2.43845E-05	-1.62276E-06	1.43431E-05	12002	1.19E-03	4.78E-03			
32	12110	-1.2104E-06	1.44512E-05	1	-2.4599E-05	1.0000001	-2.46054E-05	-1.62264E-06	1.44739E-05	12110	1.19E-03	4.78E-03			
33	12217	-1.2103E-06	1.45807E-05	1	-2.48179E-05	1.0000001	-2.48243E-05	-1.62251E-06	1.46034E-05	12217	1.19E-03	4.78E-03			
34	12324	-1.2102E-06	1.47103E-05	1	-2.50368E-05	1.0000001	-2.50432E-05	-1.62239E-06	1.47329E-05	12324	1.19E-03	4.78E-03			
35	12450	-1.21E-06	1.48628E-05	1	-2.52946E-05	1.0000001	-2.5301E-05	-1.62225E-06	1.48854E-05	12450	1.19E-03	4.78E-03			
36	12598	-1.2099E-06	1.50419E-05	1	-2.55974E-05	1.0000001	-2.56038E-05	-1.62208E-06	1.50645E-05	12598	1.19E-03	4.78E-03			
14	► ► ESH3 RESUL	TS SUMMARY	CESH3 RESU	LTS 🔬 S MAT	TRIX ESH3 🖉 ES	SH3 MEAS 🦯	ESH2 RESULTS	SUMMARY 📈 E	SH2 RESULTS	S MATRIX ESH2 SESH2 MEAS / 🗐 /		J 4			



\* (0)

### > Correction applied to $Z_{in}$ at each frequency

	А	В	С	D	E	F	G	н	1.00	J	К	L	М	N	0	Р	Q	R	S
1		MEASUR	EMENT 1	MEASUREMENT 2		MEASUREMENT 3		MEASUREMENT 4		MEASUREMENT 5		MEAN OF MEASURMENTS		UA		UB		U (k=2)	
2	FREQUENCY (Hz)	Z <sub>IN</sub>   (Ω)	φ(Z <sub>IN</sub> ) (°)	Z <sub>IN</sub>   (Ω)	$\phi(Z_{IN})$ (°)	Z <sub>IN</sub>   (Ω)	$\phi(Z_{IN})$ (°)	Z <sub>IN</sub>   (Ω)	$\varphi(Z_{\text{IN}})  (^{\circ})$	Z <sub>IN</sub>   (Ω)	φ(Z <sub>IN</sub> ) (°)	Z <sub>IN</sub>   (Ω)	$\phi(Z_{IN})$ (°)	Z <sub>IN</sub>   (Ω)	φ(Z <sub>IN</sub> ) (°)	Z <sub>IN</sub>   (Ω)	$\phi(Z_{IN})$ (°)	Z <sub>IN</sub>   (Ω)	$\phi(Z_{IN})$ (°)
3	9000	5.96	24.34	5.94	24.15	5.95	24.15	5.96	24.14	5.95	24.28	5.95	24.21	0.01	0.09	0.00	0.00	0.01	0.18
4	9107	5.97	24.29	5.97	24.35	5.98	24.35	5.97	24.35	5.97	24.40	5.97	24.35	0.00	0.04	0.00	0.00	0.01	0.08
5	9214	5.95	24.40	5.97	24.28	5.95	24.28	5.95	24.33	5.96	24.37	5.96	24.33	0.01	0.05	0.00	0.00	0.02	0.11
6	9322	5.95	24.62	5.96	24.61	5.96	24.61	5.95	24.66	5.94	24.69	5.95	24.64	0.01	0.03	0.00	0.00	0.02	0.07
7	9429	5.95	24.76	5.97	24.68	5.95	24.68	5.95	24.72	5.95	24.72	5.95	24.71	0.01	0.04	0.00	0.00	0.02	0.07
8	9536	5.94	24.81	5.95	24.95	5.95	24.95	5.95	24.87	5.94	24.90	5.95	24.90	0.01	0.06	0.00	0.00	0.01	0.12
9	9643	5.94	24.88	5.94	24.87	5.95	24.87	5.93	24.87	5.94	24.88	5.94	24.87	0.01	0.01	0.00	0.00	0.01	0.02
10	9751	5.94	25.12	5.95	25.09	5.94	25.09	5.95	25.00	5.94	25.06	5.94	25.07	0.01	0.05	0.00	0.00	0.01	0.09
11	9858	5.94	25.20	5.97	25.08	5.96	25.08	5.96	25.21	5.96	24.98	5.96	25.11	0.01	0.10	0.00	0.00	0.02	0.19
12	9965	5.95	25.25	5.96	25.14	5.96	25.14	5.96	25.14	5.95	25.41	5.96	25.22	0.01	0.12	0.00	0.00	0.01	0.23
13	10072	5.96	25.35	5.96	25.39	5.96	2!								0.05	0.00	0.00	0.01	0.10
14	10180	5.96	25.60	5.97	25.63	5.96	2! V	lagni	tude	and	bha	se co	prrec	bet	0.06	0.00	0.00	0.01	0.13
15	10287	5.95	25.77	5.95	25.78	5.96	2:	agim	uado	and	price				0.01	0.00	0.00	0.01	0.01
16	10394	5.95	25.86	5.97	25.79	5.95	25.79	5.96	25.80	5.95	25.82	5.96	25.81	0.01	0.03	0.00	0.00	0.02	0.06
17	10501	5.95	26.01	5.97	26.04	5.96	26.04	5.95	26.12	5.98	25.97	5.96	26.04	0.01	0.05	0.00	0.00	0.02	0.11
18	10608	5.97	26.24	5.98	26.13	5.98	26.13	5.96	26.20	5.96	26.17	5.97	26.17	0.01	0.05	0.00	0.00	0.02	0.10
19	10716	5.97	26.20	5.98	26.17	6.00	26.17	5.97	26.35	5.98	26.24	5.98	26.23	0.01	0.08	0.00	0.00	0.02	0.15
20	10823	5.98	26.56	5.97	26.54	5.99	26.54	5.97	26.57	5.97	26.60	5.98	26.56	0.01	0.02	0.00	0.00	0.02	0.05
21	10930	5.97	26.67	5.99	26.67	5.98	26.67	5.97	26.73	5.98	26.78	5.98	26.70	0.01	0.05	0.00	0.00	0.01	0.10
22	11037	6.00	26.90	6.00	26.85	5.99	26.85	5.99	26.98	5.99	26.92	5.99	26.90	0.00	0.05	0.00	0.00	0.01	0.11
23	11145	6.00	27.02	6.00	27.06	6.00	27.06	6.00	27.02	5.97	27.05	5.99	27.04	0.01	0.02	0.00	0.00	0.03	0.04
24	11252	5.99	27.43	6.01	27.29	6.01	27.29	5.99	27.24	6.00	27.21	6.00	27.29	0.01	0.08	0.00	0.00	0.02	0.17
25	11359	6.01	27.41	6.02	27.30	6.02	27.30	6.00	27.40	6.01	27.45	6.01	27.37	0.01	0.07	0.00	0.00	0.02	0.13
26	11466	6.00	27.74	6.01	27.69	6.01	27.69	6.00	27.73	6.01	27.76	6.01	27.72	0.01	0.03	0.00	0.00	0.02	0.06
27	11573	6.03	27.82	6.04	27.83	6.04	27.83	6.02	27.95	6.04	27.81	6.03	27.85	0.01	0.06	0.00	0.00	0.02	0.12
28	11681	6.02	27.88	6.03	27.87	6.04	27.87	6.04	27.96	6.02	27.94	6.03	27.90	0.01	0.04	0.00	0.00	0.02	0.09
29	11788	6.05	28.28	6.06	28.35	6.06	28.35	6.05	28.31	6.06	28.37	6.06	28.33	0.01	0.04	0.00	0.00	0.01	0.07
30	11895	6.05	28.48	6.05	28.46	6.07	28.46	6.05	28.45	6.04	28.52	6.05	28.48	0.01	0.03	0.00	0.00	0.02	0.06
31	12002	6.06	28.63	6.07	28.69	6.07	28.69	6.07	28.66	6.06	28.66	6.06	28.66	0.01	0.02	0.00	0.00	0.02	0.05
32	12110	6.06	28.64	6.09	28.64	6.09	28.64	6.08	28.68	6.07	28.69	6.08	28.66	0.01	0.03	0.00	0.00	0.02	0.06
33	12217	6.09	29.11	6.09	29.04	6.09	29.04	6.09	29.01	6.10	29.02	6.09	29.04	0.00	0.04	0.00	0.00	0.01	0.08
34	12324	6.09	29.16	6.09	29.18	6.10	29.18	6.10	29.19	6.10	29.12	6.10	29.17	0.00	0.03	0.00	0.00	0.01	0.06
35	12450	6.10	29.47	6.10	29.19	6.11	29.19	6.11	29.45	6.10	29.41	6.11	29.34	0.01	0.14	0.00	0.00	0.01	0.27
36	12598	6.13	29.68	6.14	29.67	6.14	29.67	6.14	29.55	5 13	29.69	6.14	29.67	0.01	0.02	0.00	0.00	0.01	0.03
М	ESH3 RESI	ULTS SUMMAR	Y / ESH3 RE	esults 🔬 s	MATRIX ESH3	ESH3 MEAS	ESH2 RES	SULTS SUMMAR	Y ESH2 R	ESULTS S	MATRIX ESH2	ESH2 MEAS							









#### Measurements with three different types of adapters





Adapter 2 BNC



Adapter 1 BNC



## Results

#### Measurements with three different types of adapters





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**Result of input impedance phase** 



Results

**Result of input impedance magnitude** 70.00 Nominal values of CISPR 16-1-2 Limits of CISPR 60.00 16-1-2 50.00 Magnitude ( $\Omega$ ) 40.00 Avec correction : Moyenne de tous les adaptateurs 30.00 Norme CIPRS 16-1-2 : limite sup Incertitude sur correction adaptateur : limite sup 20.00 Incertitude sur correction adaptateur : limite inf Norme CISPR 16-1-2 : limite inf 10.00 Norm CISPR 16-1-2 Sans correction 0.00 0.01 0.09 0.90 9.00 90.00 Frequency (MHz) **30 MHz** 



Results

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Results





Results





Results

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Results

# Results

#### Difference between ESH2-Z5 and ESH3-Z5 measurement results

Deviation between uncorrected and corrected results = 2.4° Deviation between uncorrected and corrected results = 5.5°



The length of ESH2-Z5 adapter is longer than ESH3-Z5 adapter



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## **Published Papers**

- EMC Europe 2015: "Adapter and method for improving the LISN input impedance measurement accuracy" (POSTER)
  - F. ZIADÉ, M. OUAMEUR, D. BÉLIÈRES, A. POLETAEFF, D. ALLAL, M. KOKALJ, B. PINTER, "Adapter and method for improving the LISN input impedance measurement accuracy", 2015 IEEE International Symposium on Electromagnetic Compatibility (EMC), Dresden, Germany, 16-22 Aug. 2015, pp. 1254 1259.
- Paper accepted in IEEE Transactions on Instrumentation and Measurements (August 2015): "Improvement of LISN Measurement Accuracy Based on Calculable Adapters"
  - F. ZIADÉ, M. KOKALJ, M. OUAMEUR, B. PINTER, D. BÉLIÈRES, A. POLETAEFF, D. ALLAL, "Improvement of LISN Measurement Accuracy Based on Calculable Adapters", IEEE Transactions on Instrumentation & Measurement, Vol. 65, pp. 365 - 377, Feb 2016.

